

Answer Keys

1	C	2	B	3	A	4	B	5	C	6	A	7	B
8	D	9	C	10	C	11	C	12	B	13	B	14	A
15	A	16	C	17	B	18	5.56	19	0.16	20	30	21	0.3
22	-0.25	23	D	24	D	25	B	26	B	27	A	28	B
29	A	30	C	31	B	32	D	33	D	34	A	35	A
36	10	37	2.828	38	360	39	99.8	40	C	41	D	42	B
43	A	44	B	45	D	46	1.142	47	0.125	48	628	49	0.0209
50	0.095	51	435	52	D	53	C	54	D	55	B	56	C
57	C	58	D	59	B	60	C	61	D	62	C	63	C
64	A	65	A										

Explanations:-

- Power transformer(s) are found at generating stations.
 - A very important feature of distribution transformer is all-day efficiency.
 - Pulse transformer is used for thyristor firing.
 - Isolation transformer generally has turns ratio 1 :1.

3. $r_2 = 0.018 \Omega / \text{ph}$

$x_2 = 0.08 \Omega / \text{ph}$

$S_{fl} = 0.04$

$N_r = N_s(1 - s) = 0.96 N_s$

at half full load speed, $\frac{N_r}{2} = 0.48 N_s = N_s(1 - s) \rightarrow s = 0.52$

$$T_{\text{eff}} = \left(\frac{3V^2}{\omega S} \right) \frac{1}{\left[\left(\frac{r_2}{s} \right) + x_2^2 \right]} \left(\frac{r_2}{s} \right)$$

$$\left[V_1^2 \right] \left[\frac{1}{\left(\frac{0.018}{0.04} \right)^2 + (0.08)^2} \right] \frac{0.018}{0.4} = V_2^2 \left[\frac{1}{\left(\frac{0.018}{0.52} \right)^2 + (0.08)^2} \right] \frac{0.018}{0.52}$$

$2.154V_1^2 = 4.55V_2^2$

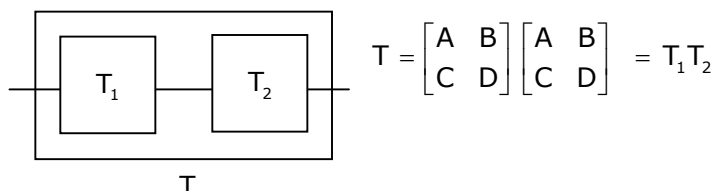
$1.466V_1 = 2.13V_2$

$\frac{V_1}{V_2} = 1.4526; \frac{V_2}{V_1} = 0.688$

% reduction = $\frac{V_1 - V_2}{V_1} = 1 - \frac{V_2}{V_1} = 1 - 0.688 = 31.15\%$

4. $L_{eq} = 4 + 8 + 6 - (2 \times 2) + (2 \times 4) = 22H$

6. $T_1 = \begin{bmatrix} A & B \\ C & D \end{bmatrix} ; T_2 = \begin{bmatrix} A & B \\ C & D \end{bmatrix}$



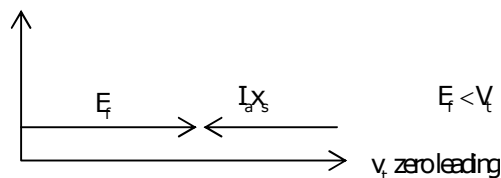
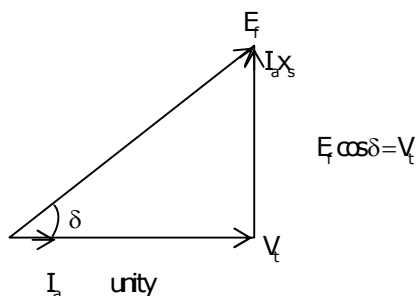
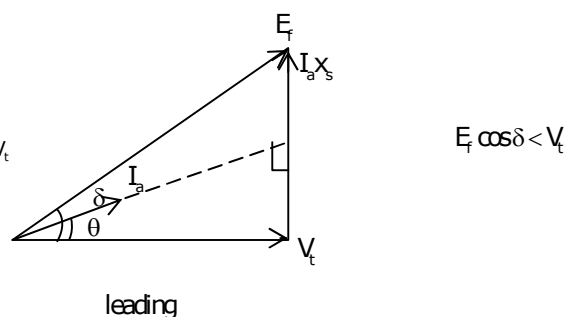
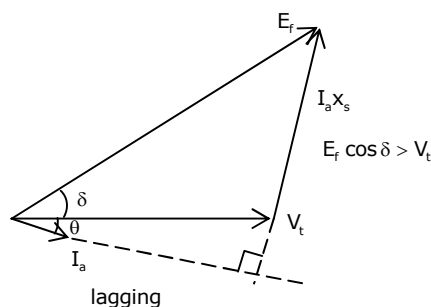
8. Error = 0 as simpon's rule gives exact value for polynomials whose degree ≤ 3

9. $f(z) = \frac{z - \sin z}{z^2} = \frac{z}{3!} - \frac{z^3}{5!} + \dots$

\therefore Re sidue of $f(z)$ at $z = 0$ is 0

$\therefore \oint_c \frac{z - \sin z}{z^2} dz = 0$

10. The phasor diagram for alternator



11. $m = 5_{gm} = 0.005\text{kg}; E_g = mc^2 = 0.005 \times (3 \times 10^2)^2$
 $E = 4.5 \times 10^{14} \text{ joules or watt - sec}$
 $= \frac{4.5 \times 10^4}{1000 \times 3600} = 12.5 \times 10^7 \text{ kWh}$

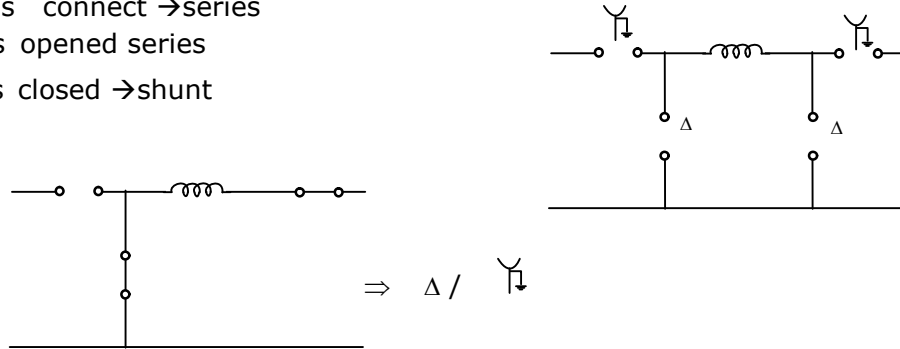
12. The zero sequence Network of Transformer representation

↘ Means connect → series

Y means opened series

Δ means closed → shunt

Here



13. $X(s) = \frac{4}{(s+2)(s+4)} = \frac{2}{s+2} - \frac{2}{s+4} \Rightarrow \text{Poles } s=-2, -4$

Given that ROC lies between lines passing through $s=-2$ and $s=-4$.

Hence $x(t)$ will be two sided signal.

$$\therefore x(t) = -2e^{-2t} \cdot u(-t) - 2e^{-4t} u(t)$$

at pole $s=-2$, $\text{Re}[s] < -2 \Rightarrow \text{Left side}$

at pole $s=-4$, $\text{Re}[s] > -4 \Rightarrow \text{Right side}$

14. $V_o = V \sin \omega t$

$$\frac{dv_o}{dt} = V\omega \cos \omega t$$

$$\text{maximum output} = V\omega = 10 \times 10^6$$

$$V = \frac{10 \times 10^6}{2 \times \pi \times 2 \times 10^6} = 0.8V$$

15. The closest scale marking w.r.t to the measured length is chosen. Here it is 231 cm (L).

Now with absolute certainty we can say that $L \pm 0.1 \text{ cm}$. since 0.1 cm is the smallest measurement quantity in this scale.

16. $P [\text{neither selected}] = \left(1 - \frac{8}{9}\right) \left(1 - \frac{5}{8}\right) = \frac{1}{24}$

17. We know that

$$M = \frac{SH}{\pi f} \Rightarrow H \propto \frac{1}{S}$$

$$\frac{H_{old}}{H_{new}} = \frac{S_{new}}{S_{old}}$$

Machine – 1

$$\frac{5}{H_{new}} = \frac{100}{400}$$

$$H_{new} = 20 \text{ MJ/MVA}$$

Machine – 2

$$\frac{5}{H_{new}} = \frac{100}{200}$$

$$H_{2 \text{ new}} = 10 \text{ MJ/MVA}$$

$$\therefore H_{eq} = 20 + 10 = 30 \text{ MJ/MVA}$$

18. $\phi_2 = 0.95\phi_1$, $E_1 = V_t$,

$$E_2 = V_t - 0.1V_t = 0.9V_t$$

$$\frac{E_1}{E_2} = \frac{\phi_1 \omega_1}{\phi_2 \omega_2} \Rightarrow \frac{1}{0.9} = \frac{1}{0.95} \times \frac{\omega_1}{\omega_2}$$

$$\Rightarrow \frac{\omega_1}{\omega_2} = \frac{0.95}{0.9} \Rightarrow \frac{\omega_1 - \omega_2}{\omega_2} = \frac{0.05}{0.9}$$

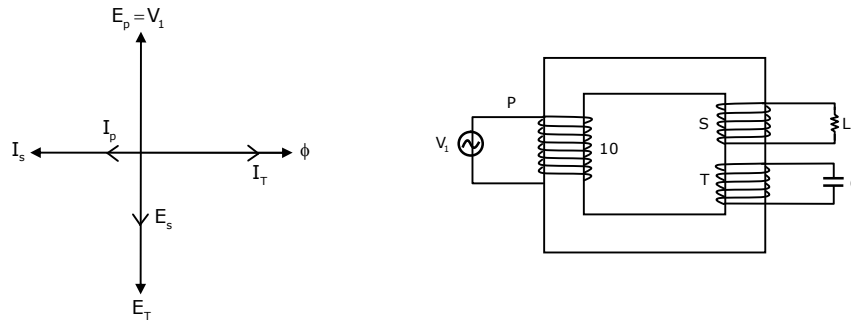
$$\Rightarrow \text{speed regulation} = 5.56\%$$

19. $w_n = \sqrt{25} = 5 \text{ rad/sec}$; $2\xi w_n = 4 \Rightarrow \xi = \frac{4}{10} = 0.4$

Damping ratio with derivative feedback control is $\xi' = \xi + \frac{w_n k_t}{2}$

$$0.8 = 0.4 + \frac{5 \cdot k_t}{2} \Rightarrow k_t = 0.16$$

20. Neglecting the magnetizing and loss components (as it is ideal transformer) the phasor diagram is



E_s = induced voltage in secondary

E_T = induced in tertiary

I_s will lag E_s by 90° (load induction)

I_T will lead E_T by 90° (load capacitive)

Secondary AT = $10 \times 50 = 500$ AT

Tertiary AT = $20 \times 40 = 800$ AT

Resultant load mmf = $(800 - 500)$ AT = 300 AT

As the primary should neutralize load mmf so primary current = $\frac{300}{10} = 30$ A

21. Overall $\eta = \frac{\text{Electrical o / p in heat units}}{\text{Heat of combustion}} = 28.66\%$

Heat equal of 1 kWh = 860 Kcal.

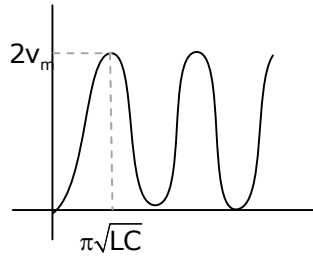
$$\therefore \text{Heat of combustion} = \frac{860}{0.2866} = 3000.69 \approx 3000 \text{ Kcal}$$

$$\therefore \text{Fuel consumption} = \frac{\text{Heat produced}}{\text{calorific value}} = \frac{3000}{10000} = 0.3 \text{ kg / kWh}$$

22. $X(z) = \left(\frac{0.5}{1 - 2z^{-1}} \right) z^{-1}$; ROC includes unit circle \Rightarrow Left handed system

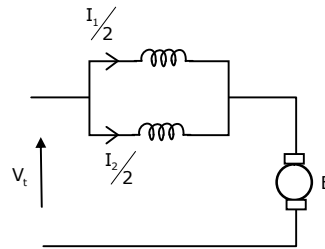
$$X(n) = -0.5(2)^{n-1} u(-n); X(0) = -\frac{1}{4} = -0.25$$

23. Restriking Voltage $v(t) = V \left(1 - \cos \frac{t}{\sqrt{LC}} \right)$



\therefore Peak value = $2V_m$; Time = $\pi\sqrt{LC}$ sec

24. $\phi_1 = K \frac{I_1}{2} + K \frac{I_1}{2} = KI_1$
 $\phi_2 = KI_2 + KI_2 = 2KI_2$
 $T_{e1} = K_a \phi_1 I_1$; $T_{e2} = K_a \phi_2 I_2$
 $T_{e1} = T_{e2} \therefore \frac{\phi_1}{\phi_2} = \frac{I_1}{2I_2} = \frac{\sqrt{2}}{2} = \frac{1}{\sqrt{2}}$
 $\Rightarrow KI_1^2 = 2KI_2^2$
 $\Rightarrow I_1 = \sqrt{2} I_2$
 $\frac{E_1}{E_2} = \frac{\phi_1 \omega_1}{\phi_2 \omega_2} \Rightarrow 1 = \frac{1 \cdot \omega_1}{\sqrt{2} \cdot \omega_2} \Rightarrow \omega_2 = \frac{\omega_1}{\sqrt{2}}$



25. Since, A is real involutory matrix
 $\therefore A^{-1}$ exists
 \therefore The equations have unique solution.

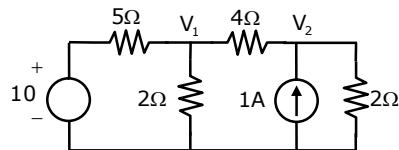
26. The power delivered to the load is = $20 \times 0.8 \text{ kW} = 16 \text{ kW}$

The transformation ratio of auto transformer $k = \frac{200}{250} = \frac{4}{5}$

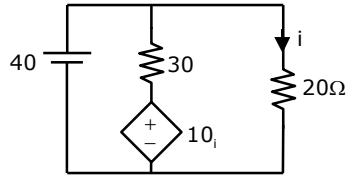
We know inductively delivered power = $(1-k) \times \text{total power delivered}$
 $= 3.2 \text{ kW}$

Conductionally delivered power = $k \times \text{total power delivered}$
 $= 12.8 \text{ kW}$

27. Annual fixed charges = $95 \times 10^5 \times 10\% = 9.5 \times 10^5$
 Total running charges = $(9 \times 10^5 + 6 \times 10^5) = 15 \times 10^5$
 Total annual cost = $(9.5 \times 10^5 + 15 \times 10^5) = 24.5 \times 10^5$
 Annual load factor = $\frac{\text{No. of units delivered}}{\text{max. demand} \times 8760}$
 \therefore No. of units delivered = $0.5 \times 40000 \times 8760 = 17.52 \times 10^7$
 \therefore cost per unit = $\frac{\text{Total annual cost}}{\text{No. of units delivered}} = \frac{24.5 \times 10^5}{17.52 \times 10^7} = 100 = 1.398 \text{ paise}$
28. Poles $f(z) = \tan z$ are given by $z = (2n+1)\frac{\pi}{2}$, n is integer and each (simple pole) denoted by 'a'.
 $\therefore \text{Res } f(z) = \frac{\sin a}{-\sin a} = -1$
 $z = a$
29. Necessary condition for the system to be linear is if $x(t) = 0 \Rightarrow y(t) = 0$
 but in $y(t) = 2x(t) + 4.5$ above condition is not satisfied. Hence the system is non-linear.
30. Slots per pole per phase $q=3$
 Slots per pole = $3 \times 3 = 9$
 So slot pitch $\gamma = \frac{180^\circ}{9} = 20^\circ$
 coil span = $8 \times 20^\circ = 160^\circ$
 Coil is short pitched by 20°
 distribution factor
 $K_d = \frac{\sin \frac{q\gamma}{2}}{q \sin \frac{\gamma}{2}} = \frac{\sin \frac{3 \times 20^\circ}{2}}{3 \sin \frac{20^\circ}{2}} = 0.959$
 pitch factor $k_p = \cos \frac{\epsilon}{2} = \cos \frac{20^\circ}{2} = 0.98$
 winding factor $k_w = k_d \cdot k_p = 0.94$
31. Applying KCL at V_1 and V_2
 $\frac{V_1 - 10}{5} + \frac{V_1}{2} + \frac{V_1 - V_2}{4} = 0 \quad \dots 1$
 $\frac{V_2 - V_1}{4} + \frac{V_2}{2} = 1 \quad \dots 2$
 By solving (1) and (2), we will get
 $V_1 = 2.7V, \quad V_2 = 2.23V$



32. $t = 0^- \quad \therefore i(0) = \frac{40}{20} = 2A$



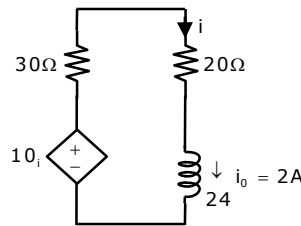
at $t = 0^+$ the circuit becomes

$$10 i(t) = 30i(t) + 20i(t) + 2 \frac{di}{dt}$$

$$2 \frac{di}{dt} + 40 i(t) = 0$$

$$i(t) = k e^{-20t}$$

$$i(t) = 2e^{-20t} \quad i(0) = 2A$$



33. Time period $T = t_{on} + t_{off} = (1 + 1.5) = 2.5 \text{ msec}$, Duty cycle $\alpha = \frac{T_{on}}{T} = \frac{1}{2.5} = 0.4$

$$\text{Form-factor (FF)} = \frac{\text{RMS Value}}{\text{Average Value}} = \frac{\sqrt{\alpha} \cdot E_{dc}}{\alpha \cdot E_{dc}} = \frac{1}{\sqrt{\alpha}} = \frac{1}{\sqrt{0.4}} = 1.58$$

$$\text{Ripple factor (RF)} = \sqrt{(\text{FF})^2 - 1} = \sqrt{\frac{1}{\alpha} - 1} = \sqrt{\frac{1 - \alpha}{\alpha}} = \sqrt{\frac{1 - 0.4}{0.4}} = 1.23$$

34. Using Green's theorem,

$$\oint x dy - y dx = 2 \times \text{area of the ellipse } 3x^2 + 2y^2 = 1 = \sqrt{\frac{2}{3}} \pi$$

35. $2y \frac{dx}{dy} = 2 - x \Rightarrow \frac{dx}{dy} + \frac{1}{2y} x = \frac{1}{y}$ is a linear equation

$$\text{IF} = e^{\int \frac{1}{2y} dy} = \sqrt{y} \therefore \text{solution is } x \cdot \sqrt{y} = \int \frac{1}{y} \sqrt{y} dy + c$$

$$= 2\sqrt{y} + c \dots\dots\dots(1), \text{passing through } (0, 1) \text{ gives } c = -2 \therefore x\sqrt{y} = 2\sqrt{y} - 2$$

36. 10 – bit Ring counter \equiv Mod – 10 counter

4 – bit parallel counter \equiv Mod – 16 counter

Mod – 25 Ripple counter \equiv Mod – 25 counter

4 – bit Johnson counter \equiv Mod – 8 counter

$$\therefore x_1 = 320 \text{ KHz} / 10 = 32 \text{ KHz}; x_2 = 32 / 16 = 2 \text{ KHz}$$

$$x_3 = 2 \text{ KHz} / 25 = 80 \text{ Hz}; x_4 = 80 \text{ Hz} / 8 = 10 \text{ Hz}$$

$$37. T(s) = \frac{C(s)}{R(s)} = \frac{16}{16 + s(s+4)};$$

$$T(j\omega) = \frac{16}{16 - \omega^2 + 4j\omega} = \frac{16}{\sqrt{(16 - \omega^2)^2 + (4\omega)^2}} \angle -\tan^{-1}\left(\frac{4\omega}{16 - \omega^2}\right)$$

$$\frac{d}{d\omega} \sqrt{(16 - \omega^2)^2 + (4\omega)^2} = 0 \Rightarrow \frac{d}{d\omega} \sqrt{\omega^4 - 16\omega^2 + 256} = 0$$

$$4\omega^3 - 32\omega = 0 \rightarrow \omega = \sqrt{8} = 2\sqrt{2} \text{ rad / sec} = 2.828 \text{ rad / sec}$$

$$38. \text{ For Inductor } Q_{sh} = \frac{V^2}{\omega L_{ph}}$$

$$\therefore Q_{sh} \propto V^2$$

$$\frac{Q_{sh1}}{Q_{sh2}} = \left(\frac{V_1}{V_2}\right)^2 = \frac{50}{40.5} = \left(\frac{400/\sqrt{3}}{V_2 / Ph}\right)^2$$

$$\Rightarrow \frac{V_2}{ph} = 207.84 \text{ kV}; V_2 = \sqrt{3} \times 207.8 = 360 \text{ kV}$$

39. voltmeter resistance

$$R_v = V_{FSD} \times \text{sensitivity} = 10 \times 10 = 100 \Omega$$

$$R_m = 0.2 \Omega$$

$$R_s = 100 - 0.2 = 99.8 \Omega$$

40. The pole zero pattern given in the figure is an all pass filter

$$41. k_a \cdot \frac{d\phi}{dt} = c(t) \text{ Taking Laplace transform } E(s) = k_a s \phi(s) \Rightarrow \frac{E(s)}{\phi(s)} = k_a \cdot s$$

42. $p = \frac{1}{100}, n = 15 \text{ and } \lambda = \frac{15}{100} = 0.15$

$$P[\text{atmost one defective tyre}] = P(X = 0) + P(X = 1)$$

$$= e^{-0.15}(1 + 0.15) \text{ (using poisson distribution)}$$

$$= e^{-0.15}(1.15)$$

Approximate number of lots containing atmost one deective tyre

$$= 100 \times e^{-0.15}(1.15) = 69.75 \approx 70$$

43. Nullity of $A=1 \Rightarrow \text{rank of } A=2$

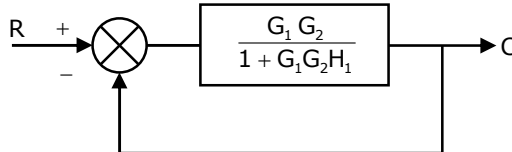
$$\Rightarrow |A| = 0 \Rightarrow k = 4$$

44. $I = \int_0^\infty \int_y^\infty \frac{e^{-x}}{x} dx dy$

$$\Rightarrow I = \int_0^\infty \int_0^x \frac{e^{-x}}{x} dy dx \text{ (using change of order of integration)}$$

$$= \int_0^\infty e^{-x} dx = 1$$

45.



$$\frac{C}{R} = \frac{G_1 G_2}{1 + G_1 G_2 H_1 + G_1 G_2}$$

46. When fault occurs, the line is isolated, after sometime by auto reclosing the breaker is closed (from data)

$$P_{\max} = \frac{EV}{x_{\text{eq}}}$$

$$x_{\text{eq}} = 0.25 + (0.4 \parallel 0.04) + 0.6$$

$$= 0.25 + 0.2 + 0.6 = 1.05$$

$$P_{\max} = \frac{1.2 \times 1.0}{1.05} = 1.142$$

47. Method - 1 $\Delta I = \frac{V_s D(1-D)}{f_L} = \frac{100 \times 0.5 \times 0.5}{1000 \times 20 \times 10^{-3}} = 0.125A$

Method-2

$$I_{\max} = \frac{V_s}{R} \left[\frac{1 - e^{-\frac{\tan}{T_a}}}{1 - e^{-\frac{T}{T_a}}} \right] = 20 \left[\frac{1 - e^{-0.0125}}{1 - e^{-0.025}} \right] = 10.062499$$

$$V_s = 100$$

$$R = 5\Omega$$

$$T_a = \frac{L}{R} = \frac{0.2}{5} = \frac{1}{25}$$

$$t_{on} = 500 \times 10^{-6}$$

$$\frac{t_{on}}{T_a} = \frac{500 \times 10^{-6}}{\frac{1}{25}} = 0.0125$$

$$\frac{T}{T_a} = \frac{10^{-3}}{\frac{1}{25}} = 0.025$$

48. Efficiency $\eta = \frac{V_2 I_2 \cos \theta_2}{V_2 I_2 \cos \theta_2 + P_c + P_{cu}}$

At rated condition

$$V_2 I_2 = 30 \text{ KVA}$$

$$\therefore 0.95 = \frac{30 \times 0.8}{30 \times 0.8 + P_c + P_{cu}} \quad \text{and} \quad 0.95 = \frac{30 \times \frac{1}{2} \times 1}{30 \times \frac{1}{2} \times 1 + P_c + \left(\frac{1}{2}\right)^2 P_{cu}}$$

Solving 2 equations, core-loss $P_c = 0.632 \text{ k}$

Ohmic-loss at rated condition $P_{cu} = 0.628 \text{ kW}$

49. pu value of $r_e = \frac{\text{ohmic loss at rated condition}}{\text{Rated VA}}$

$$= \frac{628}{30000} = 0.0209$$

50. Given $N_v = 5.4$; $N_H = 9.2$

$$\frac{\text{volt}}{\text{div}} = 50 \times 10^{-3}; \frac{\text{sec}}{\text{div}} = 1 \times 10^{-3}$$

$$V_{\text{rms}} = \frac{V_{p-p}}{2\sqrt{2}} \quad V_{p-p} = N_v \frac{\text{volt}}{\text{div}} = 5.4 \times 50 \times 10^{-3} = 0.27 \text{ V}$$

$$\therefore V_{\text{rms}} = \frac{0.27}{2\sqrt{2}} = 95.45 \text{ mv} = 0.0954 \text{ V}$$

51. Given $N_V=5.4$; $N_H= 9.2$

$$\frac{\text{volt}}{\text{div}} = 50 \times 10^{-3} ; \frac{\text{sec}}{\text{div}} = 1 \times 10^{-3}$$

$$\text{Frequency, } f = \frac{1}{T_{1c}}$$

$$T_{2c} = N_H \frac{\text{Time}}{\text{div}} = 9.2 \times 1 \times 10^{-3} = 9.2 \text{ msec}$$

$$T_{1c} = \frac{9.2}{4} = 2.3 \text{ msec}$$

$$f = \frac{1}{2.3 \times 10^{-3}} = 434.78 = 435 \text{ Hz}$$

52. Characteristic equation is

$$s^4 + 20s^3 + 15s^2 + 2s + k = 0$$

By R - H table

s^4	1	15	k
s^3	20	2	0
s^2	$\frac{298}{20}$	k	0
s^1	$(29.8 - 20k) \frac{20}{298}$	0	
s^0	k		

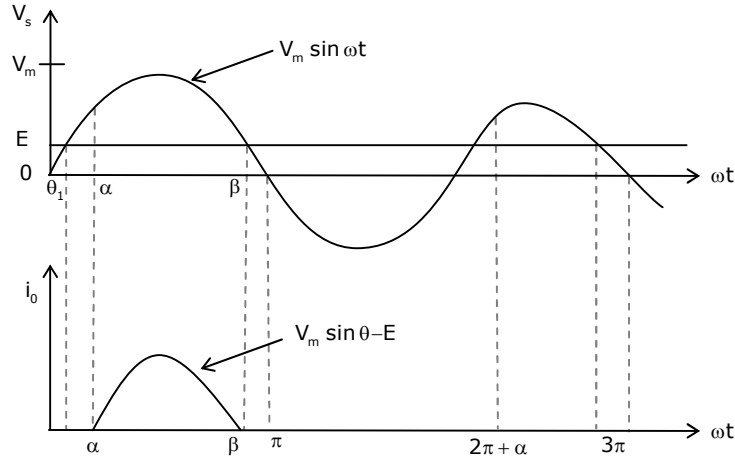
$$29.8 - 20k > 0 \Rightarrow k < \frac{29.8}{20} \Rightarrow k < 1.49$$

53. $K = 1.49$

Auxiliary equation becomes

$$\begin{aligned} \frac{298}{20} s^2 + k &= 0 \Rightarrow 14.9s^2 + 1.49 = 0 \Rightarrow -\omega^2 14.9 = -1.49 \Rightarrow \omega \\ &= \sqrt{0.1} = 0.316 \text{ rad / sec} \end{aligned}$$

54 & 55.



Min firing angle to turn on SCR is θ_1

$$V_m \sin \theta_1 = E$$

$$(240\sqrt{2}) \sin \theta_1 = 200 \rightarrow \theta_1 = 36.104^\circ$$

$$\text{Max firing angle} = \beta = \pi - \theta_1 = 36.104^\circ$$

Given firing angle α is 45° ($\alpha > \theta_1$)

The battery charging requires only the average current I_0

$$I_0 = \left(\frac{1}{R}\right) \frac{1}{2\pi} \int_{\alpha}^{\beta} [V_m \sin \theta - E] dQ = \frac{1}{2\pi R} \left[V_m \cos \theta \Big|_{\beta}^{\alpha} - E(-\alpha + \beta) \right]$$

$$I_0 = \frac{1}{2\pi R} [V_m (\cos \alpha - \cos \beta) - E(\beta - \alpha)]$$

$$\therefore I_0 = \frac{1}{2\pi \times 10} \left[240\sqrt{2} [\cos 45 - \cos 143.896] - 200 [143.896 - 45] \frac{\pi}{180} \right]$$

$$= \frac{1}{20\pi} [514.22 - 345.212] = 2.67 \text{ A}$$

$$\begin{aligned}
 V_s &= \frac{V_m}{\sqrt{2}}, V_s^2 = \frac{V_m^2}{2} \\
 I_{or} &= \frac{1}{2\pi} \int_{\alpha}^{\beta} \left(\frac{V_m \sin \theta - E}{R} \right)^2 d\theta \\
 &= \frac{1}{2\pi R^2} \left[\int_{\alpha}^{\beta} [V_m^2 \sin^2 \theta + E^2 - 2V_m E \sin \theta] d\theta \right] \\
 &= \frac{1}{2\pi R^2} \left[V_s^2 (1 - \cos^2 \theta) + E^2 - 2V_m E \sin \theta \right] \\
 &= \frac{1}{2\pi R^2} \left[V_s^2 \left(\theta - \frac{\sin^2 \theta}{2} \right) \Big|_{\alpha}^{\beta} + E^2 (\beta - \alpha) - 2V_m E \cos \theta \Big|_{\alpha}^{\beta} \right] \\
 &= \frac{1}{2\pi R^2} \left[V_s^2 (\beta - \alpha) - \frac{V_s^2}{2} [\sin 2\beta - \sin 2\alpha] - 2V_m E (\cos \alpha - \cos \beta) \right] \\
 &= \frac{1}{2\pi (10)^2} \left[(240^2 + 200^2) \frac{[143.9 - 45]\pi}{180} - \frac{240^2}{2} [\sin(2 \times 143.9) - \sin(2 \times 45)] \right. \\
 &\quad \left. - 2 \cdot (240\sqrt{2}) 200 [\cos 45 - \cos 143.9] \right] \\
 &= \frac{1}{200\pi} [168470.3495 + 56221.32 - 205696.34] \Rightarrow I_{or} = \sqrt{30.23A} = 5.5A
 \end{aligned}$$

Power delivered to $R_L = EI_0 + I_{or}^2 R = 200 \times 2.67 + 5.5^2 \times 10 = 836.5W$

Supply p.f = $\frac{\text{Power delivered to load}}{[\text{Source voltage } V_s] [\text{RMS value of source current } I_{or}]} = \frac{836.5}{240 \times 5.5} = 0.6337 \text{ lag}$

60. Possible cases:

1st Case: 2 men & 2 women

2nd case: 3 men & 1 women

3rd Case: 4 men only

Required number of ways = $6c_2 \times 5c_2 + 6c_3 \times 5c_1 + 6c_4$

62. Banti is 80% more efficient than Anand

Assume, Anand efficiency is 100 percent

Then, Banti is 180 (100+80) percent efficient

\therefore Ratio of time taken by Anand and Banti = $180:100 = 9:5$

(Reciprocal to efficiencies)

Now, assume Banti takes x days

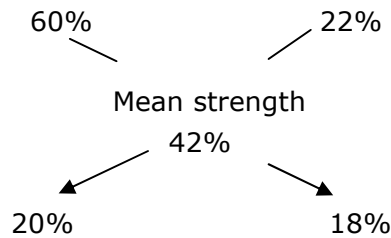
Given Anand does the job in 14 days

$14 : X :: 9:5 \Rightarrow 9x = 70$

$x = \frac{70}{9} = 7\frac{7}{9}$

63. By the rule of alligation, we have

Strength of first jar Strength of second jar



$$\text{Ratio} = 20 : 18 = 10 : 9$$

$$\therefore \text{Required quantity replaced} = \frac{9}{19}$$

64. $(x^n + 1)$ is divisible by $(x + 1)$, when n is odd

$(87^{65} + 1)$ will be divisible by 88

$(87^{65} + 1) + 86$, when divided by 88 will give 86 as remainder

65. Number of males in U.P. = $\left[\frac{3}{5} \text{ of } (15\% \text{ of } N) \right] = \frac{3}{5} \times \frac{15}{100} \times N = \frac{9N}{100}$

Where $N = 3276000$

Number of males in M.P. = $\left[\frac{3}{4} \text{ of } (20\% \text{ of } N) \right] = \frac{3}{4} \times \frac{20}{100} \times N = \frac{15N}{100}$

Number of males in Goa = $\left[\frac{3}{8} \text{ of } (12\% \text{ of } N) \right] = \frac{3}{8} \times \frac{12}{100} \times N = \frac{4.5N}{100}$

Total males in these 3 states = $(9 + 15 + 4.5) \frac{N}{100} = \frac{28.5N}{100}$

$$\text{Required \%} = \left(\frac{28.5 \times \frac{N}{100} \times 100}{N} \right) \% = 28.5\%$$